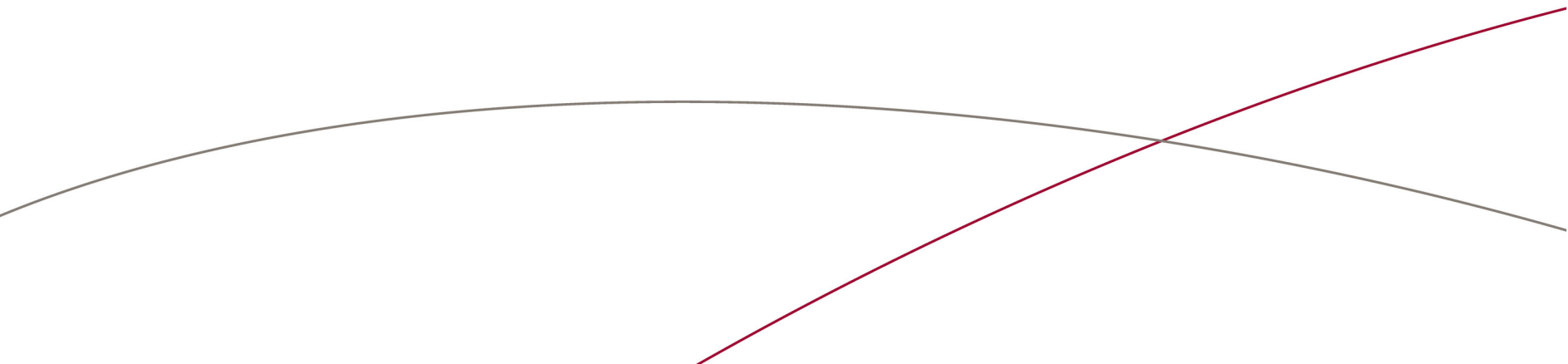




Lecture 5. Laminar Premixed Flames

Structures and Propagation



Premixed flames



Premixed flames causing coal mine explosion



A mine explosion in the Ukraine resulted in 36 dead, 14 missing, and this guy looking very terrible indeed. The explosion was methane gas, and they were mining coal. August 2001. <http://cellar.org/showthread.php?t=452>

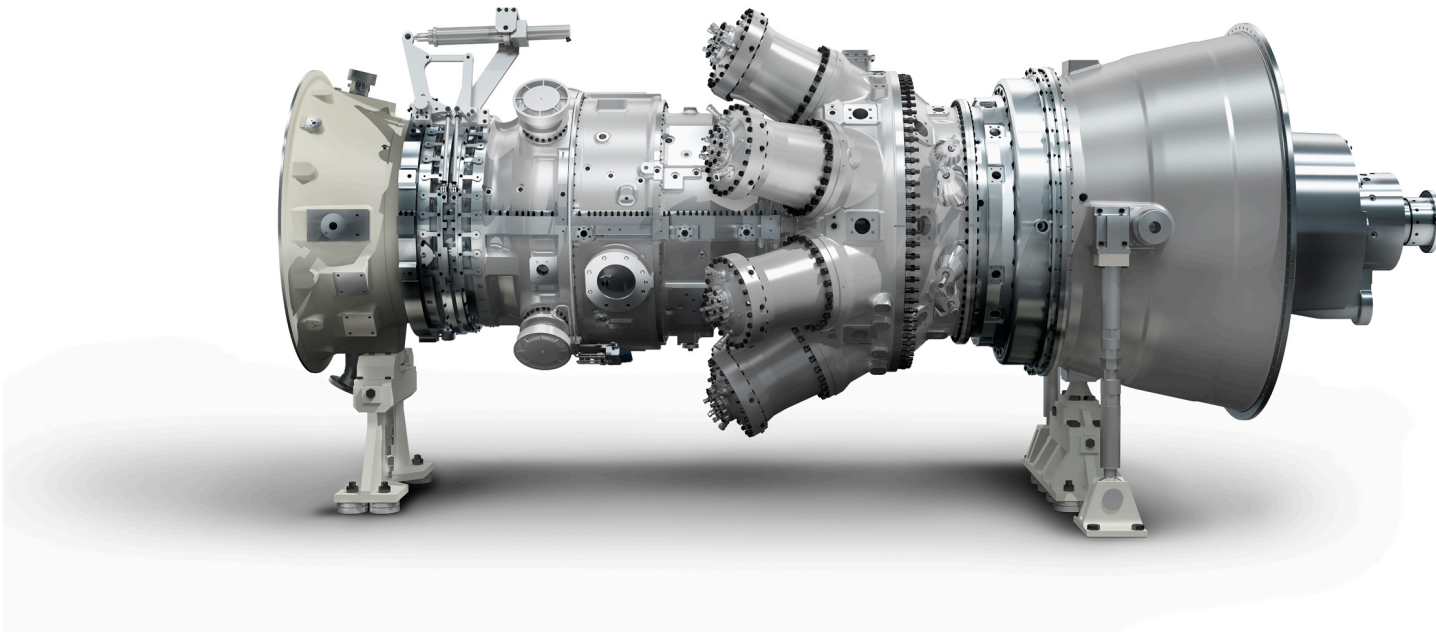




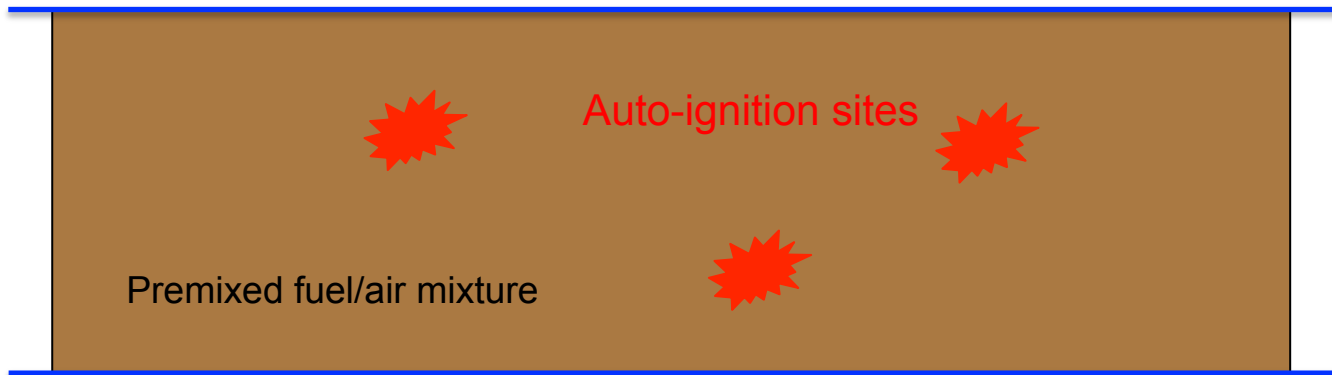
SGT-750

37 MW, 40%

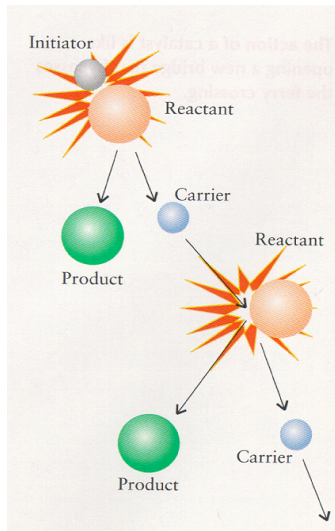
Launched nov 2010



Premixed fuel/air mixture: auto-ignition

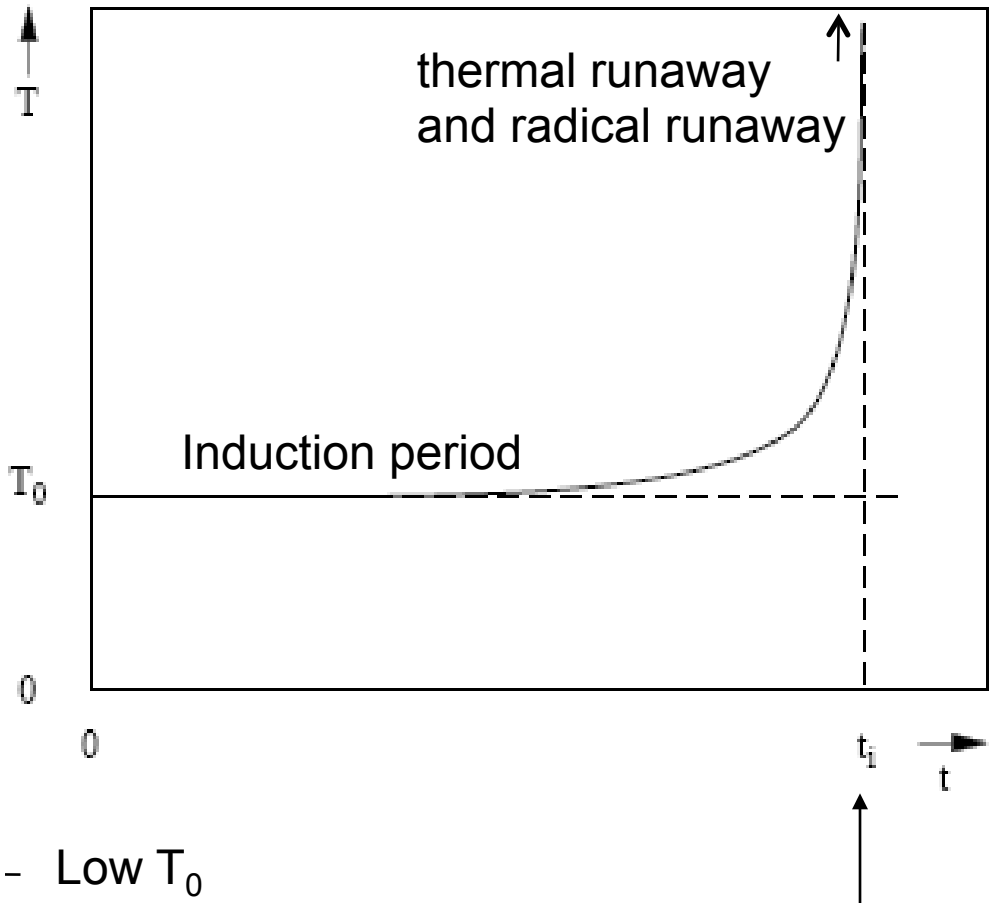
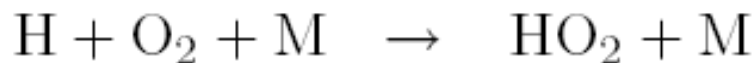
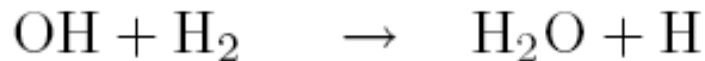
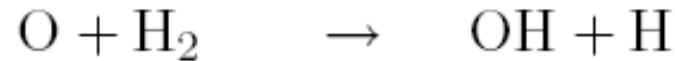
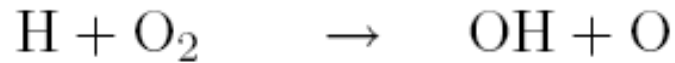


Hydrogen/air auto-ignition



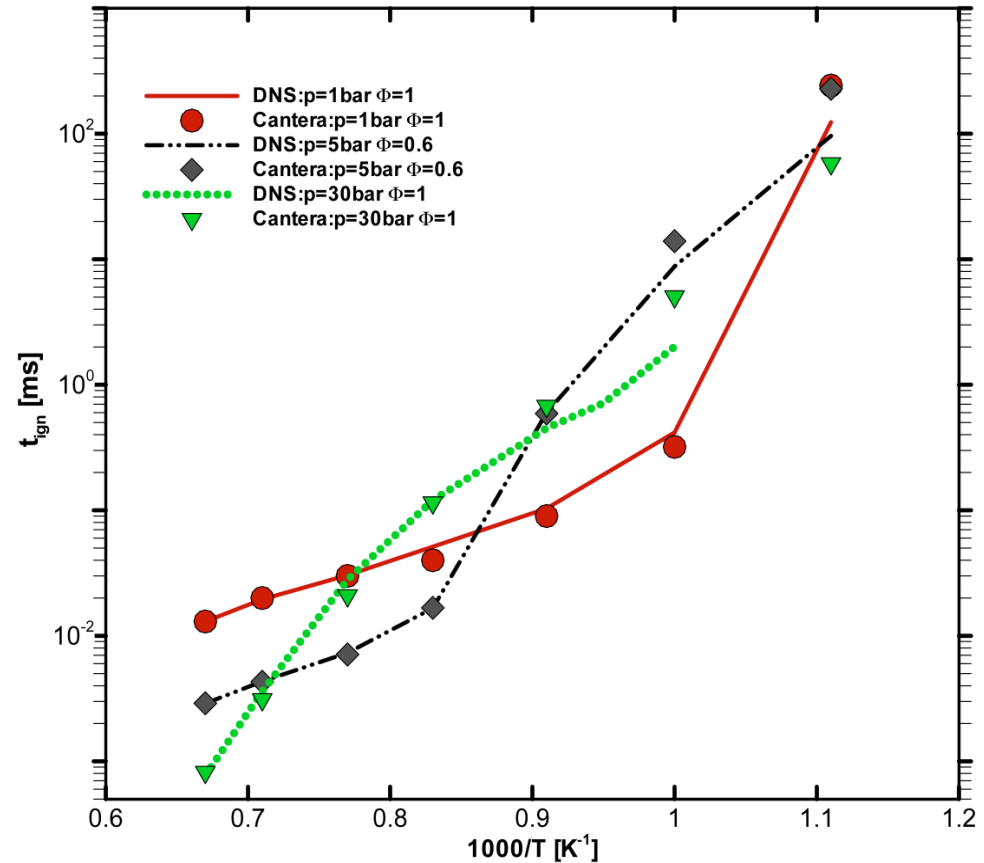
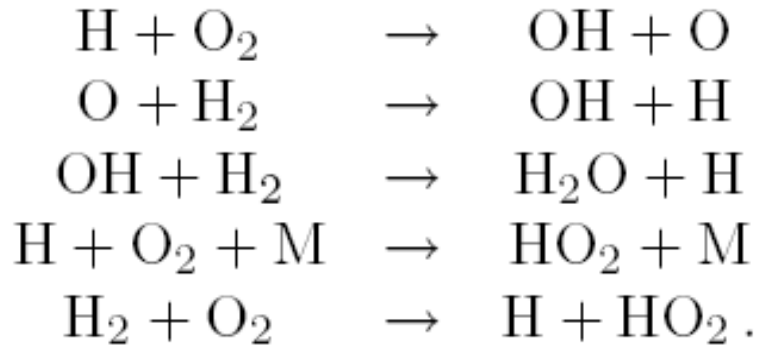
Initial temperature

→ T_0



Ignition delay time

Hydrogen/air auto-ignition

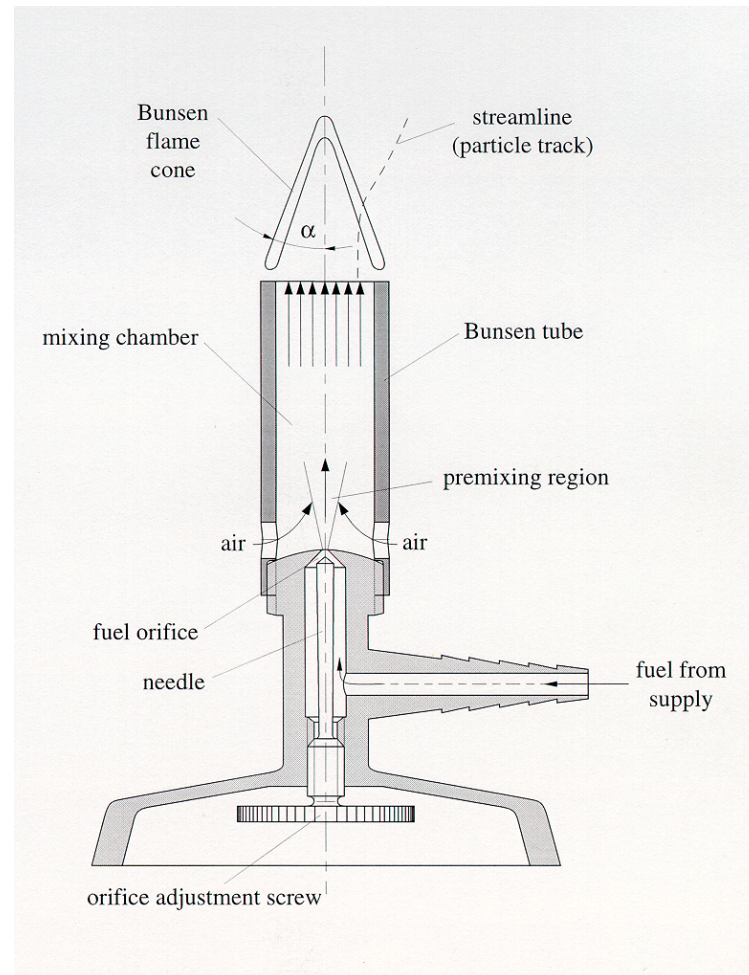


Ignition delay time of H₂/air mixture

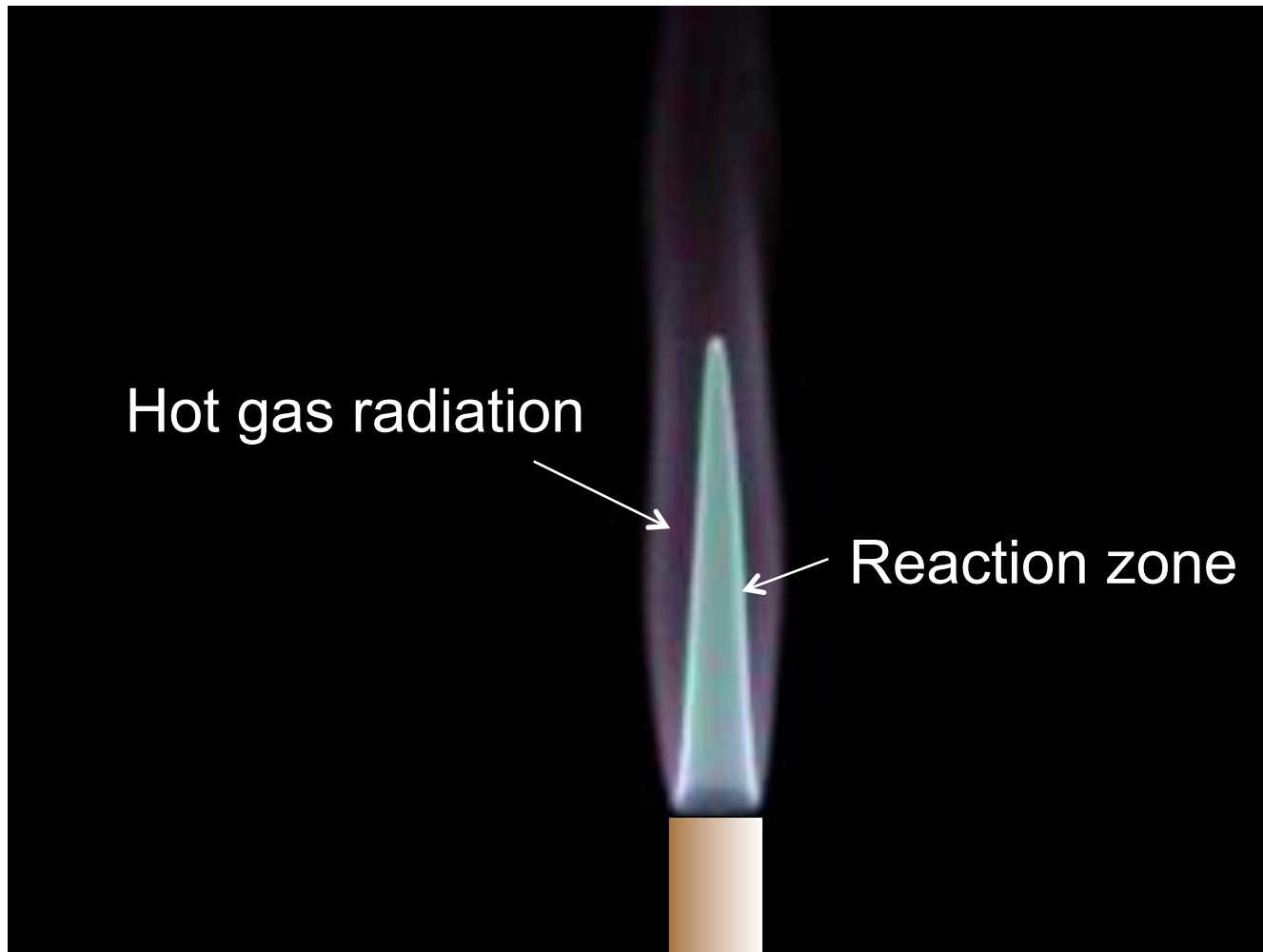
Structures and propagation of laminar premixed flames

- Structures of laminar premixed flames
- Burning velocity of laminar premixed flames
- Propagation of laminar premixed flames in flow field
- Stabilization of premixed flames
- Laminar premixed flame instability

Laminar premixed flames: Bunsen burner



Laminar premixed flames

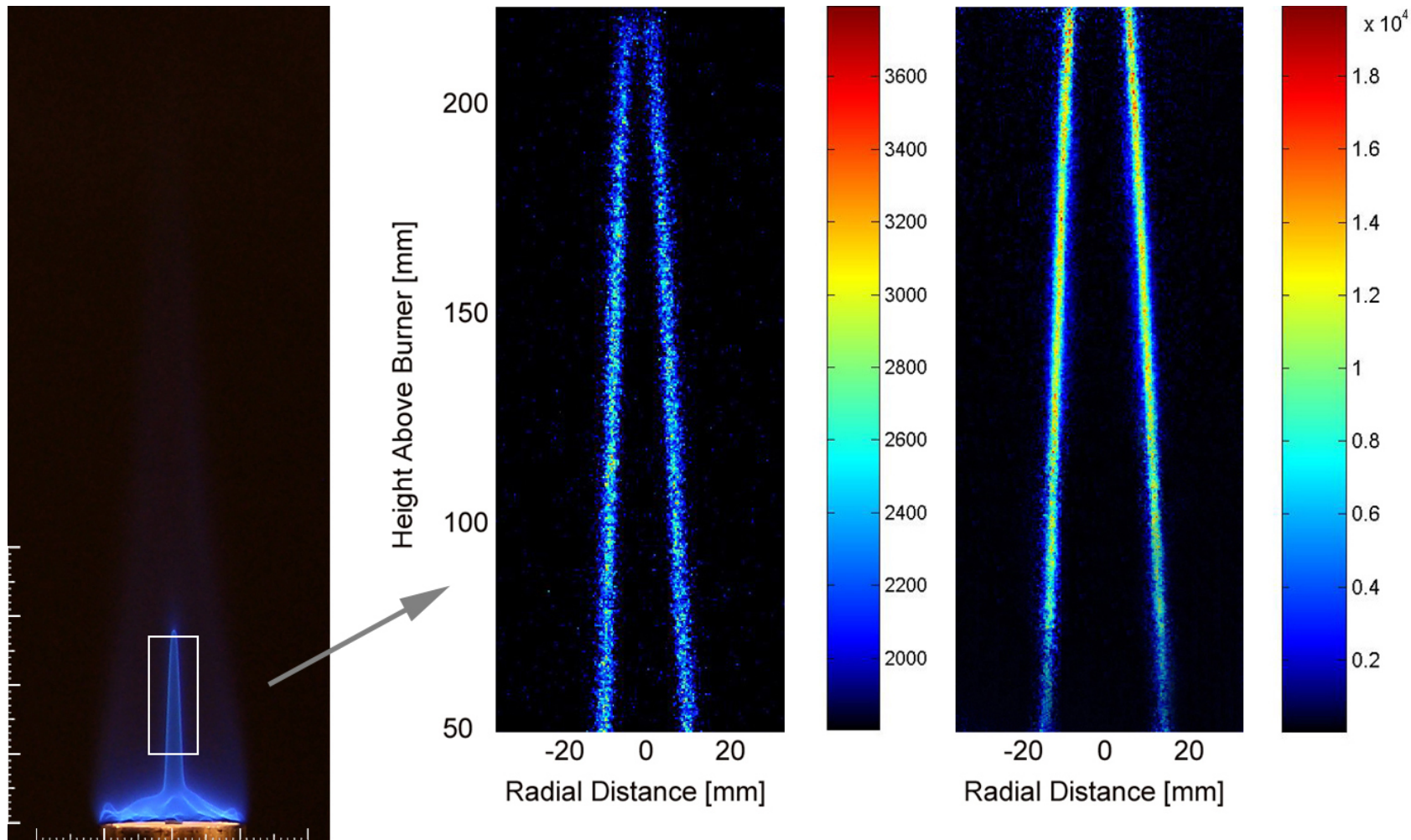


Experimental observations of flames

photo

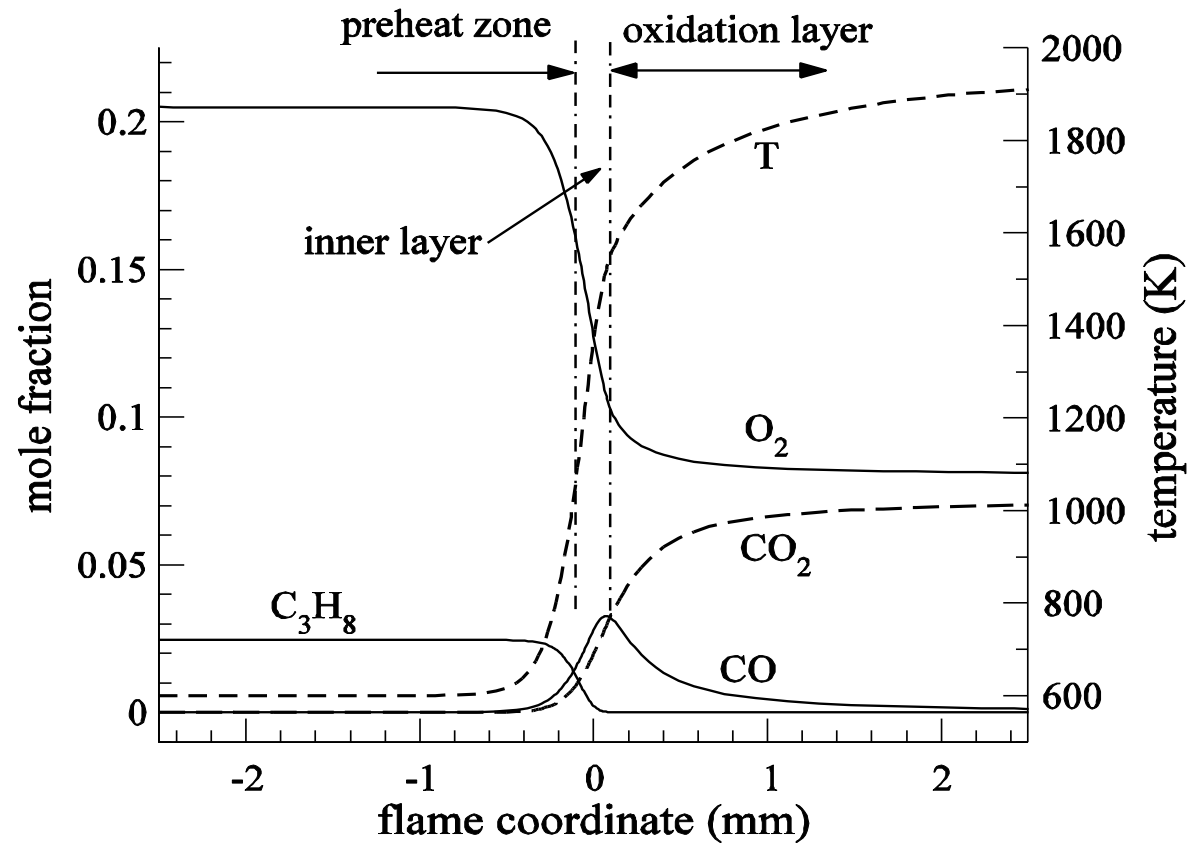
CH₂O

CH

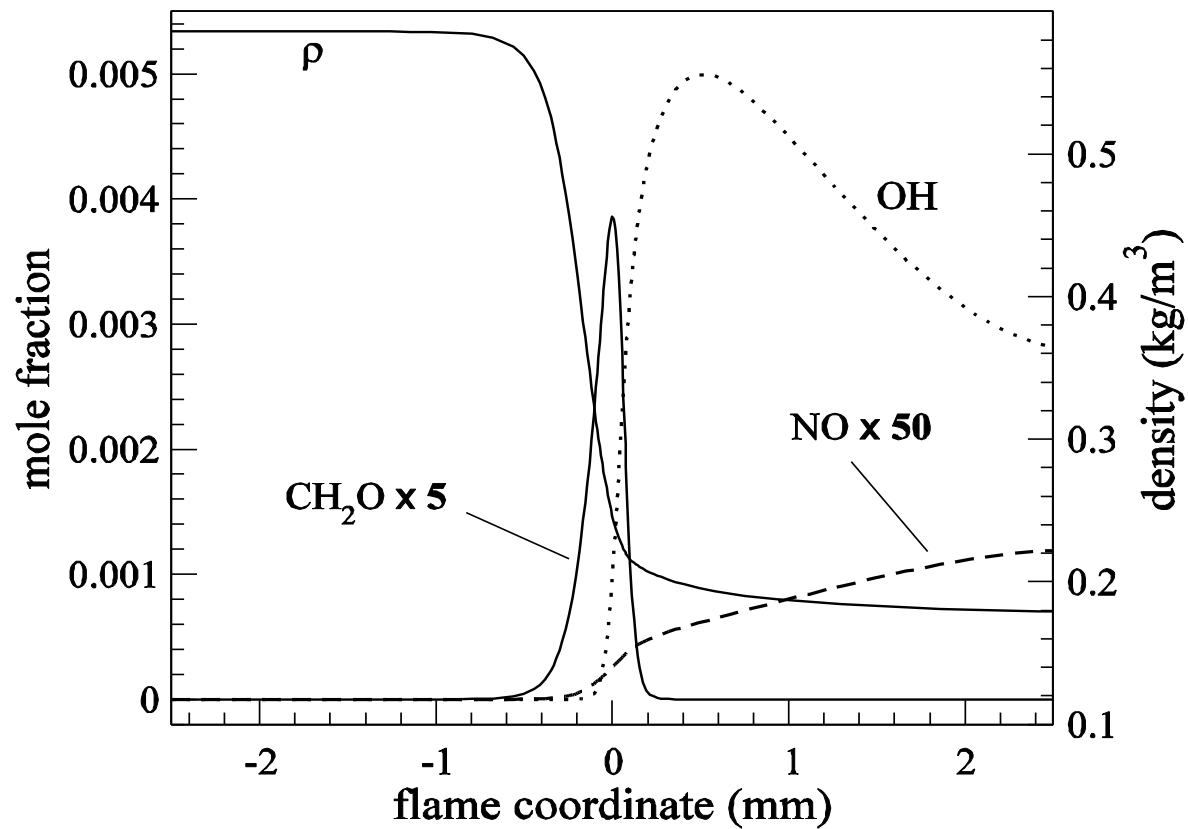


$V_o=0.45$ m/s, $\phi=1.17$; $V_{in}=11$ m/s, $\phi=1.1$

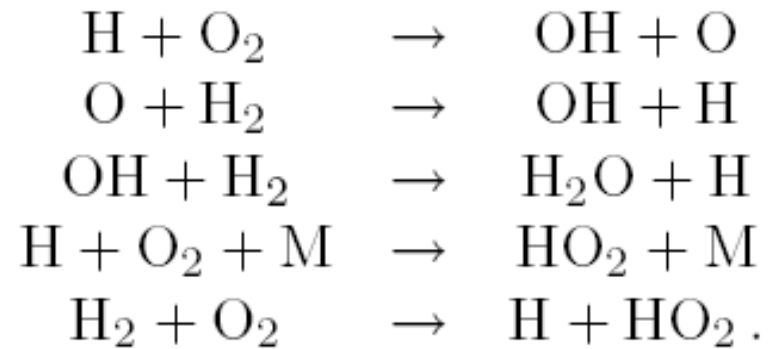
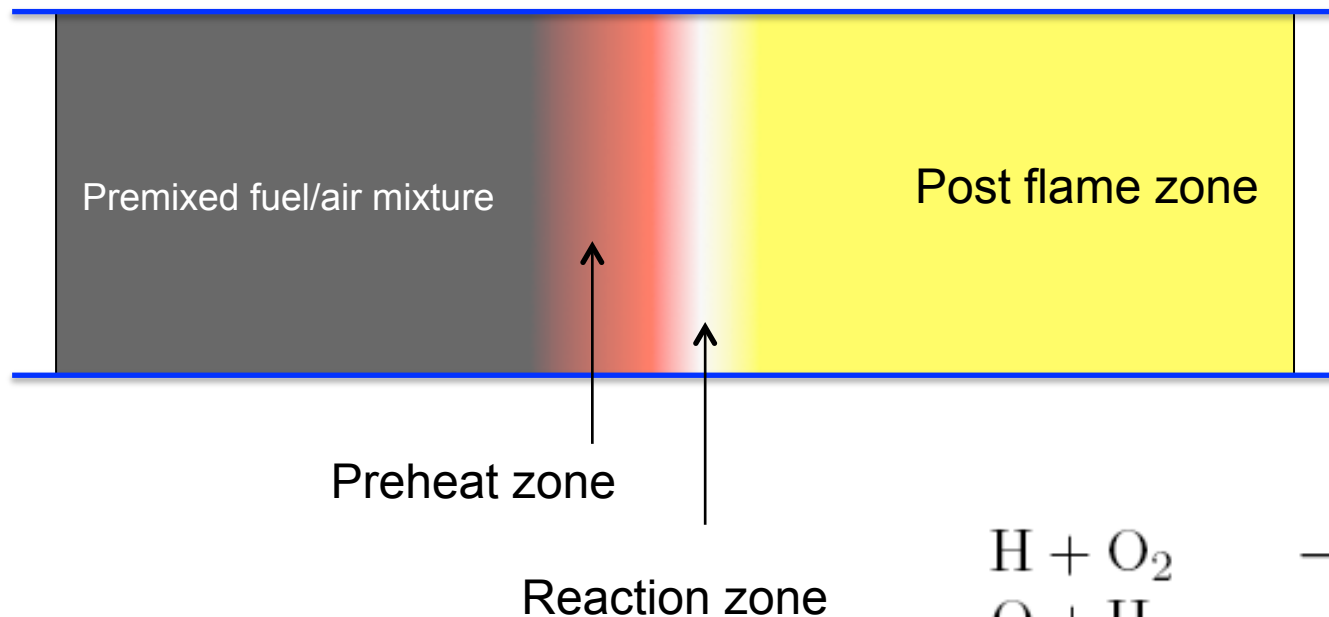
Structure of premixed flames



Structure of premixed flames



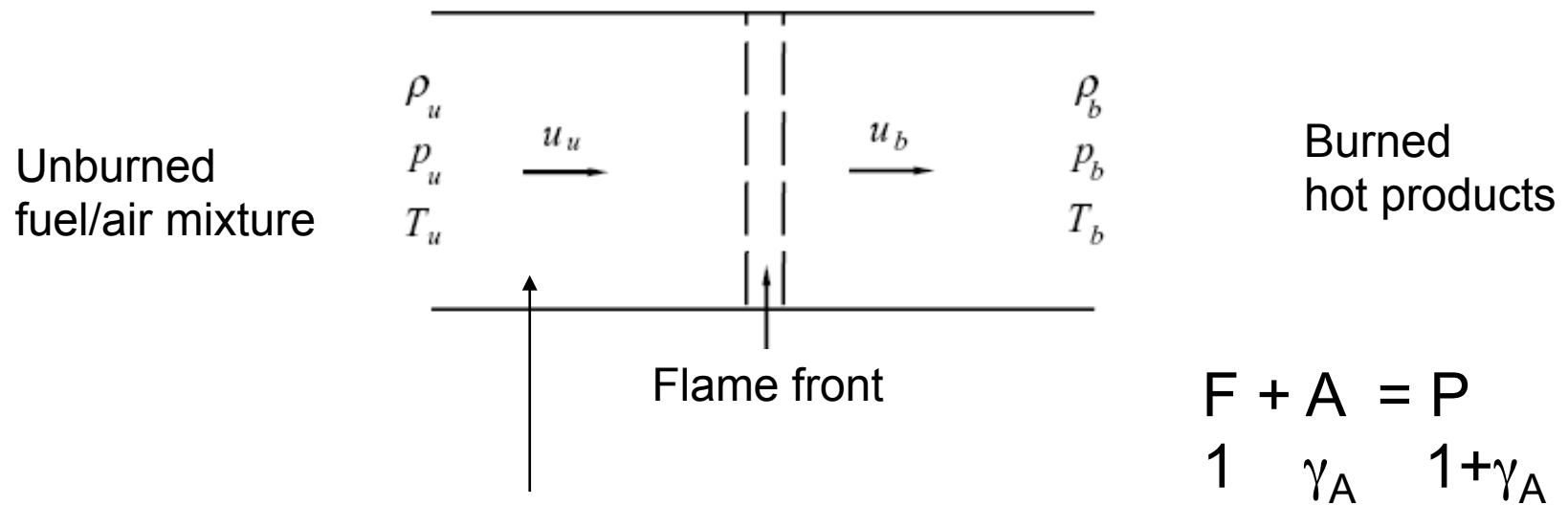
Premixed fuel/air mixture: flame propagation



Structure of premixed flames

- Preheat zone: heating up the reactants
- Inner-layer: radical formation
- Oxidation-layer: finishing the remaining reactions
- Post-flame zone: hot products, NO_x formation

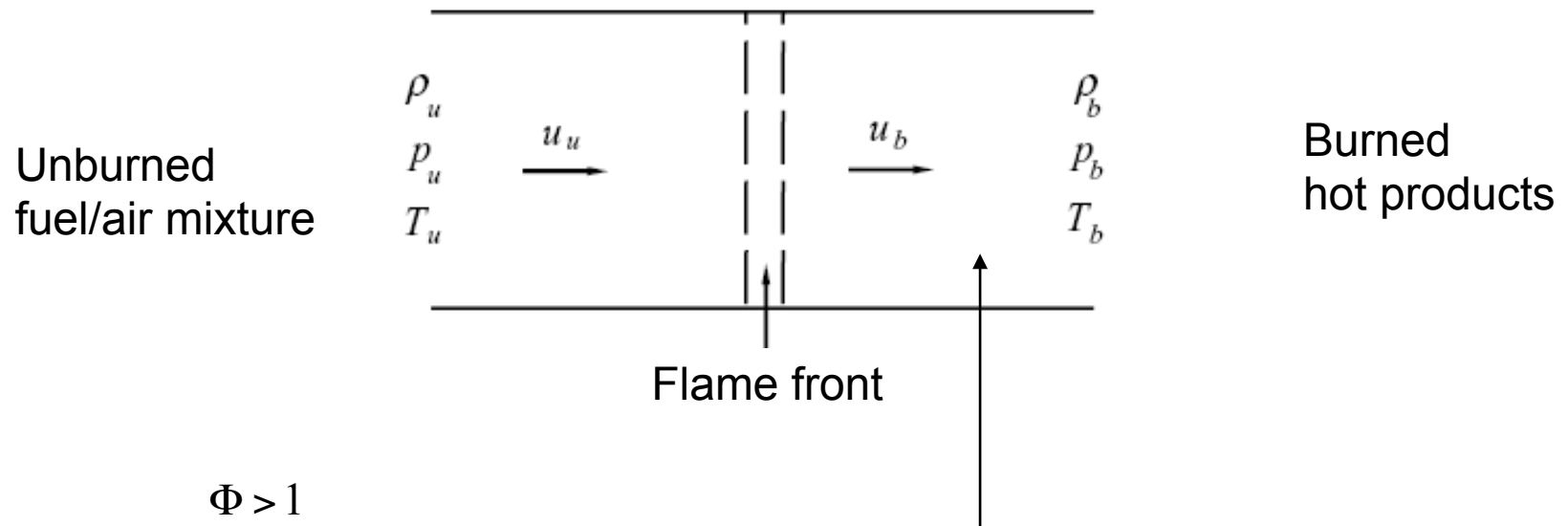
Analysis of flames: the post-flame zone



$$Y_{F,u} / Y_{A,u} = \Phi / \gamma_A, \text{ and } Y_{F,u} + Y_{A,u} = 1$$

$$Y_{F,u} = \frac{\Phi}{\Phi + \gamma_A}, \quad Y_{A,u} = \frac{\gamma_A}{\Phi + \gamma_A}, \quad \text{and } Y_{O,u} = \frac{0.233\gamma_A}{\Phi + \gamma_A}, \quad Y_{N,u} = \frac{0.767\gamma_A}{\Phi + \gamma_A},$$

Analysis of flames: the post-flame zone



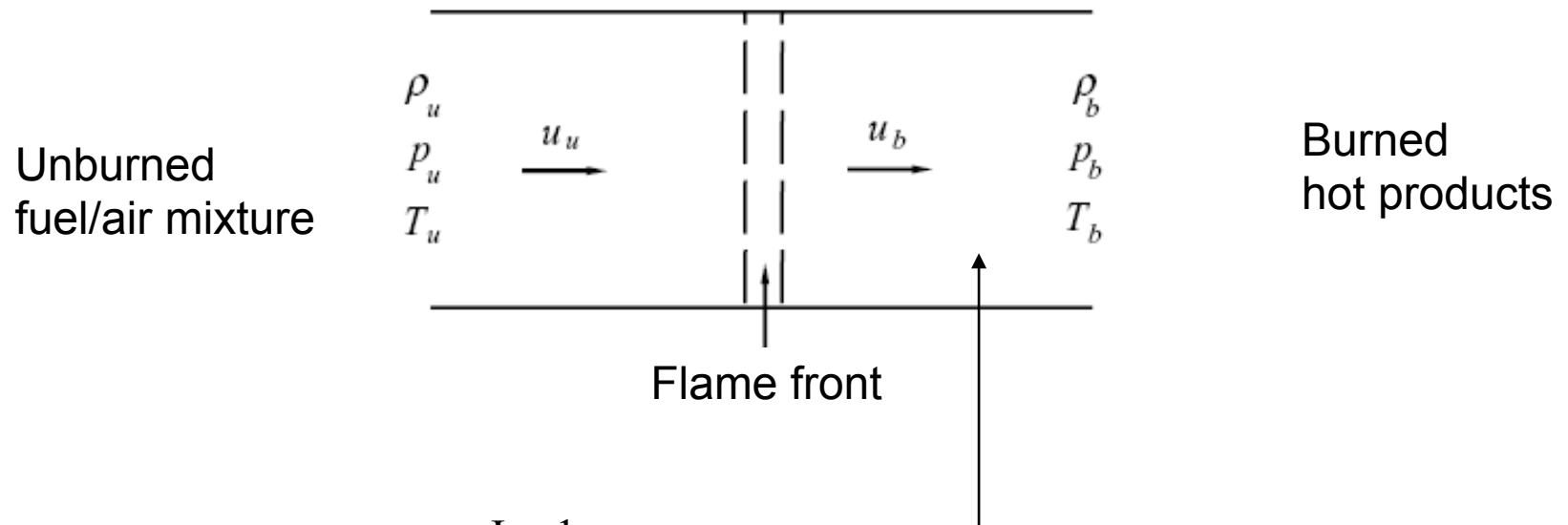
$$\Phi > 1$$

$$Y_{F,b} = Y_{F,u} - Y_{A,u} / \gamma_A = (\Phi - 1) Y_{A,u} / \gamma_A = Y_{F,u} \frac{\Phi - 1}{\Phi} = \frac{\Phi - 1}{\Phi + \gamma_A},$$

$$Y_{O,b} = 0, Y_{N,b} = Y_{N,u} = \frac{0.767 \gamma_A}{\Phi + \gamma_A}$$

$$Y_{P,b} = 1 - Y_{F,b}, P \text{ includes } N$$

Analysis of flames: the post-flame zone



$$\Phi < 1$$

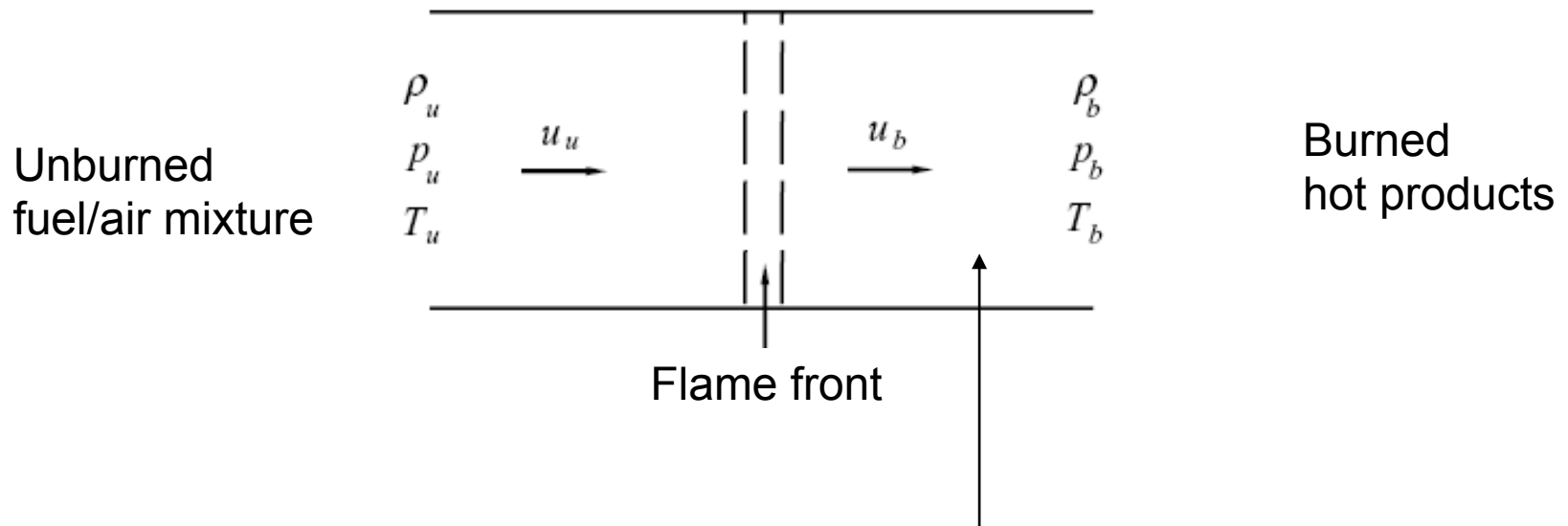
$$Y_{F,b} = 0$$

$$Y_{A,b} = Y_{A,u} - \gamma_A Y_{F,u} = (1 - \Phi) Y_{A,u} = \gamma_A Y_{F,u} \frac{1 - \Phi}{\Phi} = \gamma_A \frac{1 - \Phi}{\Phi + \gamma_A},$$

$$Y_{P,b} = 1 - Y_{A,b}$$

Both A and P
include N

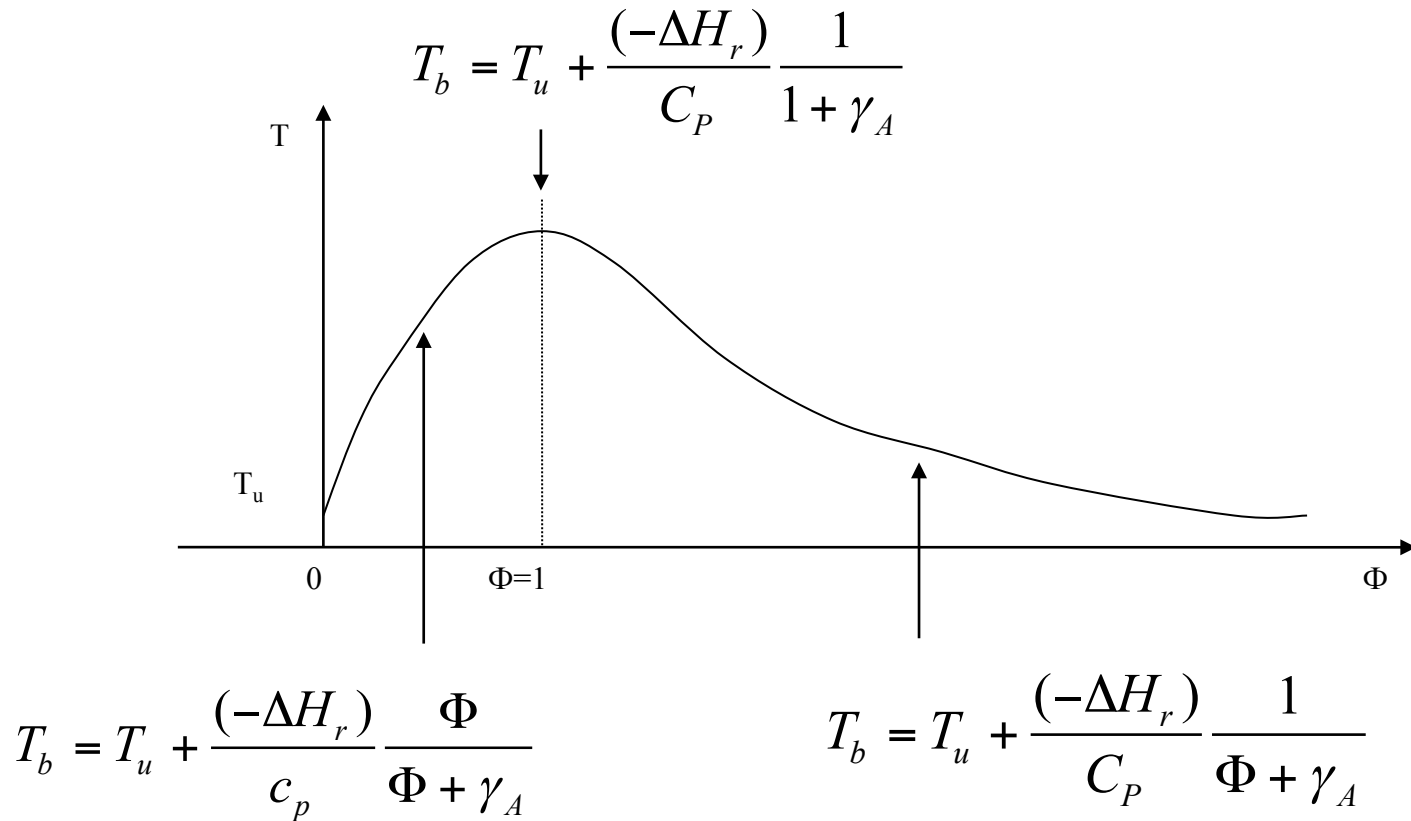
Analysis of flames: the post-flame zone



$$h_u = Y_{F,u}[h_F^0 + c_{p,F}(T_u - T_{ref})] + Y_{A,u}[h_A^0 + c_{p,A}(T_u - T_{ref})]$$

$$h_b = Y_{F,b}[h_F^0 + c_{p,F}(T_b - T_{ref})] + Y_{A,b}[h_A^0 + c_{p,A}(T_b - T_{ref})] + Y_{P,b}[h_P^0 + c_{p,b}(T_b - T_{ref})]$$

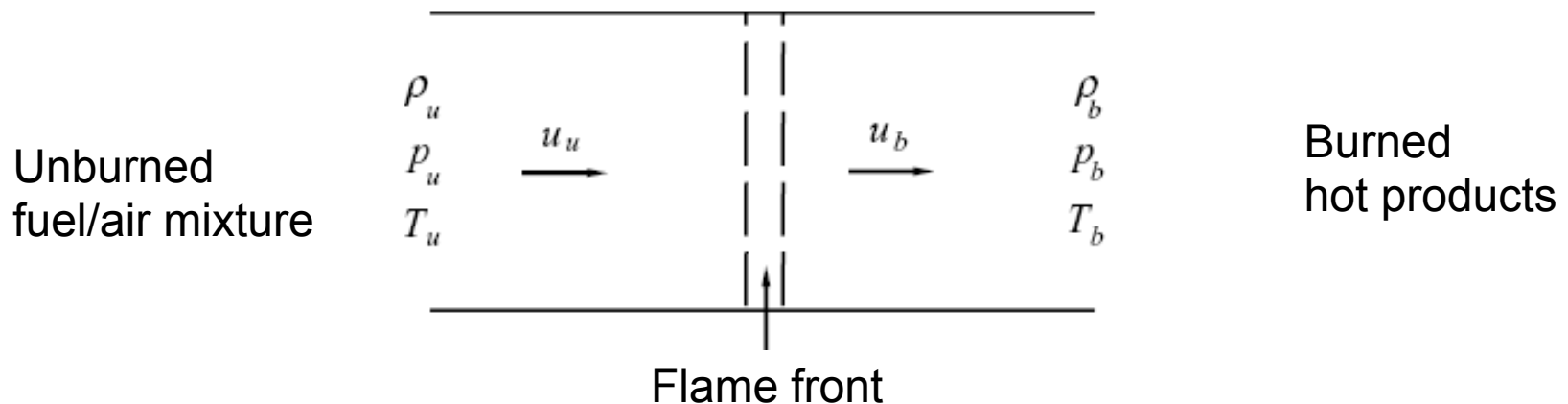
Analysis of flames: the post-flame zone



Laminar burning velocity

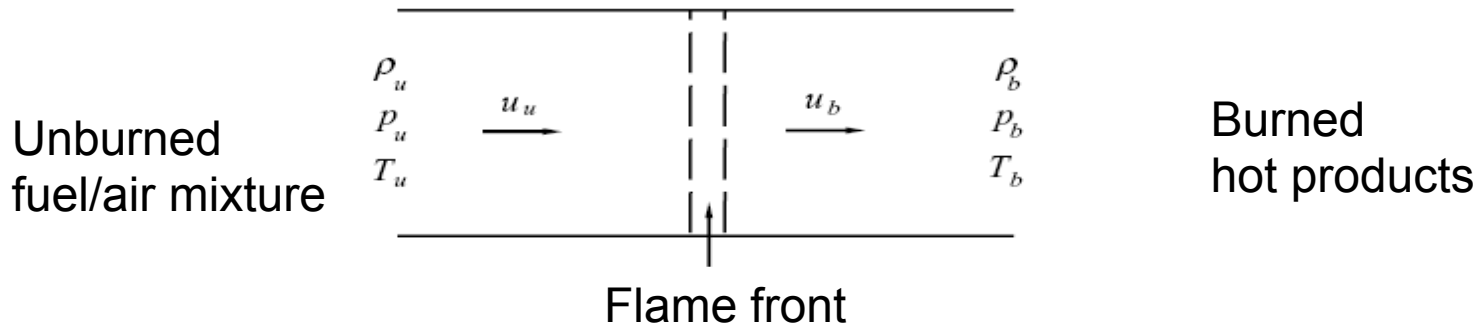
- How fast can a laminar flame propagate?
- What is the mechanism of flame propagation?
- What are the influencing factors?

Laminar burning velocity



Laminar burning velocity (also called laminar flame speed): the speed at which the flame front propagates towards the unburned mixture

Derivation of laminar burning velocity



$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \vec{v} = 0$$

$$\frac{\partial \rho Y_i}{\partial t} + \nabla \cdot \rho Y_i \vec{v} = \nabla \cdot \rho D_i \nabla Y_i + \omega_i$$

$$\rho \frac{\partial \vec{v}}{\partial t} + \rho \vec{v} \cdot \nabla \vec{v} = \nabla \cdot (pI + \tau)$$

$$\rho \frac{Dh}{Dt} - \frac{Dp}{Dt} = \nabla \cdot \left(\rho \alpha \nabla h - \rho \alpha \sum_{i=1}^N \left(1 - \frac{1}{Le_i} \right) h_i \nabla Y_i \right) + \dot{Q}_r + \tau : \nabla \vec{v}$$

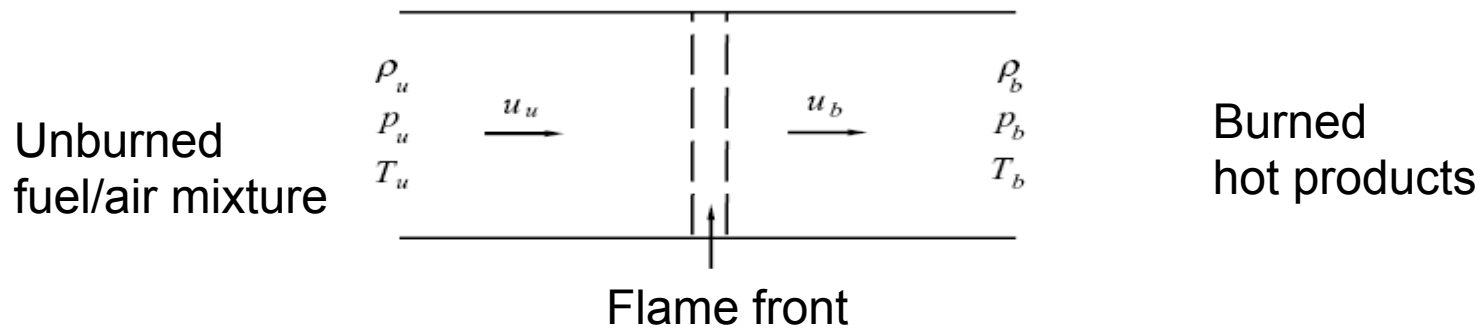
Assumptions

- 1 D
- steady state
- unity Lewis number
- low Mach number

Development of flame speed theory

- Mallard:
 - Ann Mines 7, 355 (1875)
- Mallard & Le Chatelier:
 - Ann Mines 4, 274 (1883)
- Zeldovich, Frank-Kamenetskii (1938) and Semenov (1940)
- Bernard Lewis and G Von Elbe (1937)
- Peters, Seshadri, Williams (1990s)

Derivation of laminar burning velocity



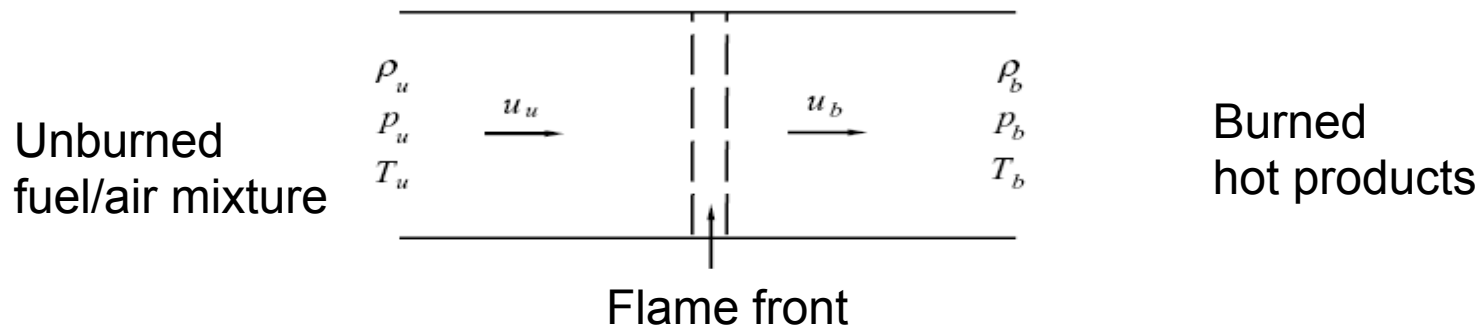
$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \vec{v} = 0$$

$$\frac{\partial \rho Y_i}{\partial t} + \nabla \cdot \rho Y_i \vec{v} = \nabla \cdot \rho D_i \nabla Y_i + \omega_i$$

Assumptions

- 1 D
- steady state
- unity Lewis number
- low Mach number

Derivation of laminar burning velocity



Assumptions

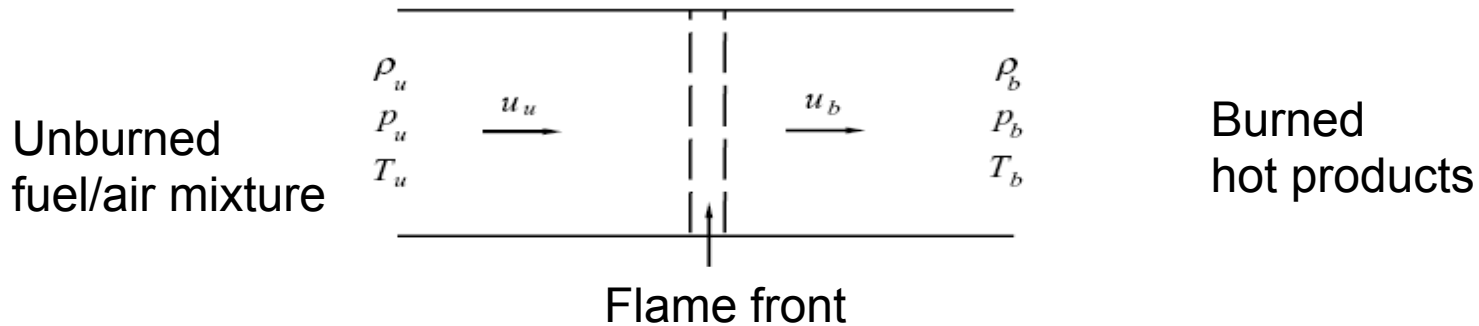
- 1 D
- **steady state**
- unity Lewis number
- low Mach number

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \vec{v} = 0$$

$$\frac{\partial \rho Y_i}{\partial t} + \nabla \cdot \rho Y_i \vec{v} = \nabla \cdot \rho D_i \nabla Y_i + \omega_i$$

0

Derivation of laminar burning velocity



Assumptions

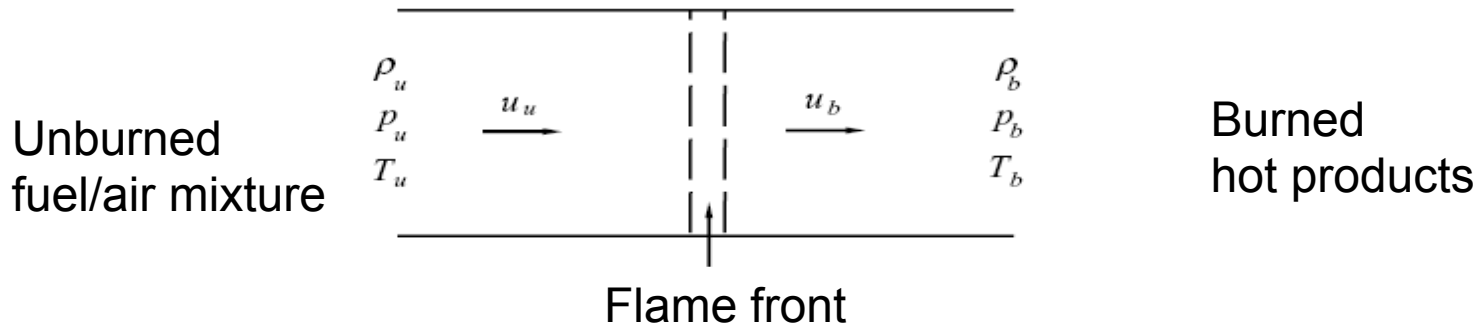
-1 D

- steady state
- unity Lewis number
- low Mach number

$$0 \left(\frac{\partial \rho}{\partial t} + \frac{d\rho u}{dx} = 0 \right)$$

$$0 \left(\frac{\partial \rho Y_i}{\partial t} + \frac{d\rho Y_i u}{dx} = \frac{d}{dx} \left(\rho D_i \frac{dY_i}{dx} \right) + \omega_i \right)$$

Derivation of laminar burning velocity



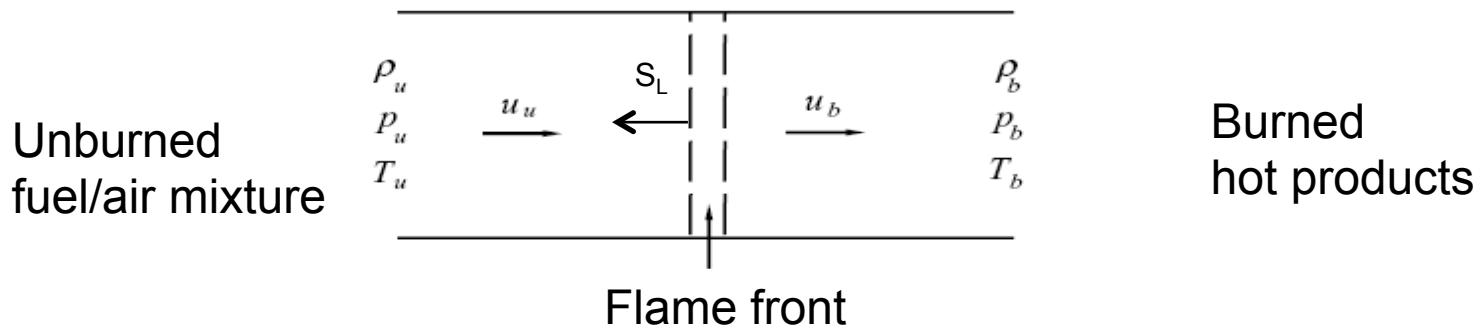
Assumptions

- 1 D
- steady state
- unity Lewis number
- low Mach number

$$0 \rightarrow \frac{\partial \rho}{\partial t} + \frac{d\rho u}{dx} = 0$$

$$0 \rightarrow \frac{\partial \rho Y_i}{\partial t} + \frac{d\rho Y_i u}{dx} = \frac{d}{dx} \left(\rho D \frac{dY_i}{dx} \right) + \omega_i$$

Derivation of laminar burning velocity



Assumptions

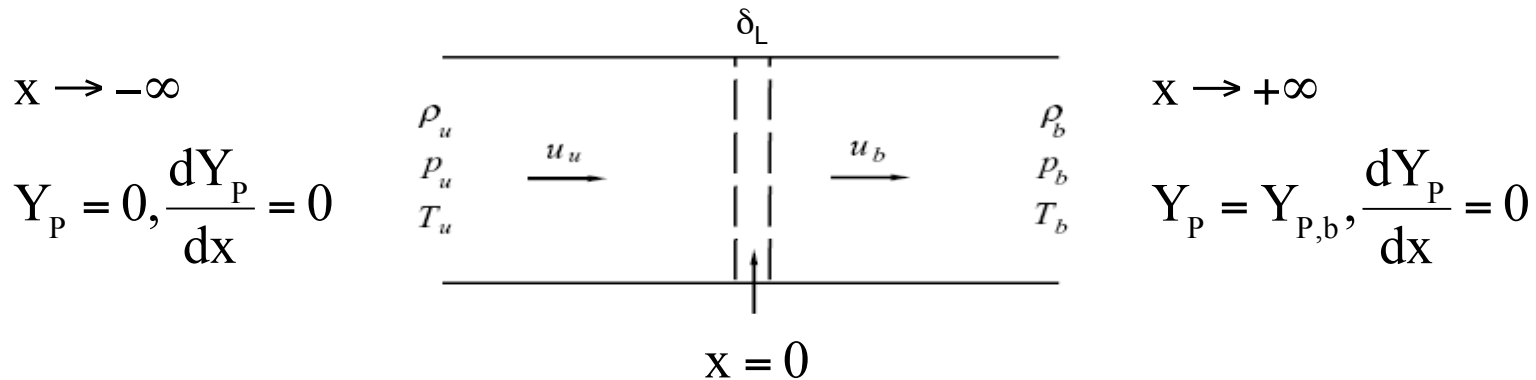
- 1 D
- steady state
- unity Lewis number
- low Mach number

$$\cancel{\frac{\partial \rho}{\partial t}} + \frac{d\rho u}{dx} = 0$$

0 $\Rightarrow \rho u = \rho_u S_L = \text{constant}$

$$\cancel{\frac{\partial \rho Y_i}{\partial t}} + \frac{d\rho Y_i u}{dx} = \frac{d}{dx} \left(\rho D \frac{dY_i}{dx} \right) + \omega_i \Rightarrow \rho_u S_L \frac{dY_i}{dx} = \frac{d}{dx} \left(\rho D \frac{dY_i}{dx} \right) + \omega_i$$

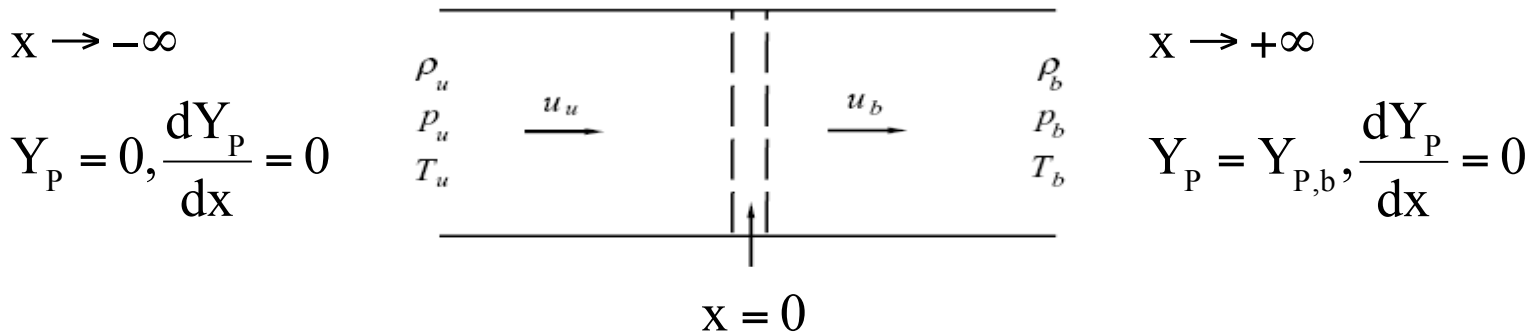
Derivation of laminar burning velocity



$$\rho_u S_L \frac{dY_i}{dx} = \frac{d}{dx} \left(\rho D \frac{dY_i}{dx} \right) + \omega_i \Rightarrow \int_{-\infty}^{+\infty} \left(\rho_u S_L \frac{dY_i}{dx} \right) dx = \int_{-\infty}^{+\infty} \left(\frac{d}{dx} \left(\rho D \frac{dY_i}{dx} \right) + \omega_i \right) dx$$

$$\Rightarrow \rho_u S_L (Y_{P,b} - 0) = \bar{\omega}_P \delta_L \Rightarrow S_L \propto \Omega \delta_L$$

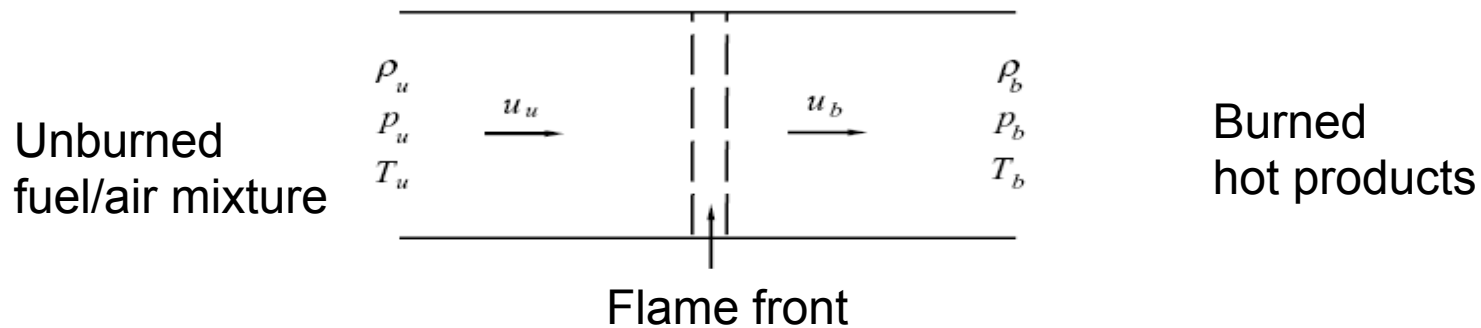
Derivation of laminar burning velocity



$$\rho_u S_L \frac{dY_i}{dx} = \frac{d}{dx} \left(\rho D \frac{dY_i}{dx} \right) + \omega_i \Rightarrow \int_{-\infty}^{-\delta_L/2} \left(\rho_u S_L \frac{dY_i}{dx} \right) dx = \int_{-\infty}^{-\delta_L/2} \left(\frac{d}{dx} \left(\rho D \frac{dY_i}{dx} \right) + \omega_i \right) dx$$

$$\Rightarrow \rho_u S_L (Y_{P,b} / 2 - 0) = \rho D \frac{Y_{P,b} - 0}{\delta_L} \Rightarrow S_L \delta_L \propto D$$

Derivation of laminar burning velocity



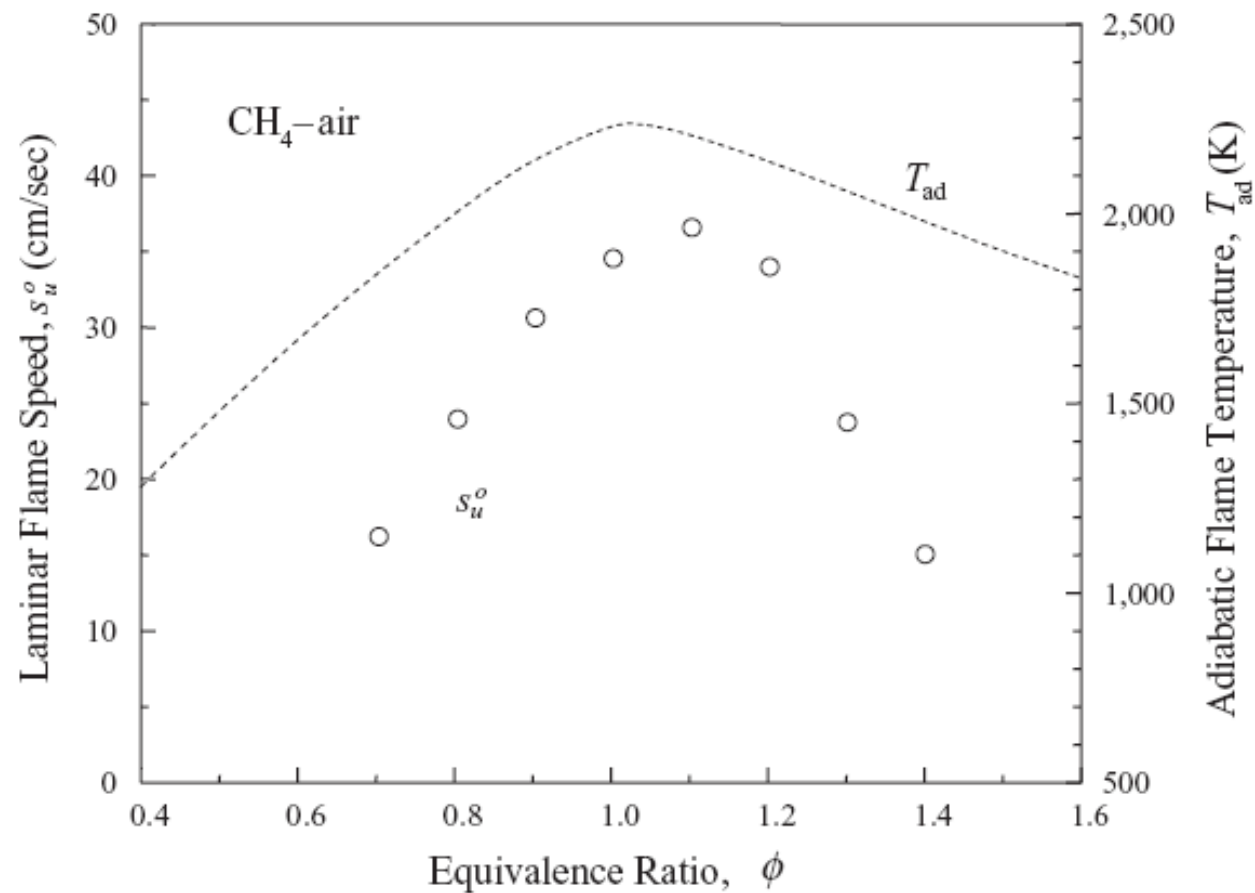
$$S_L \sim \sqrt{D\Omega},$$

$$\delta_L \sim \sqrt{D/\Omega}$$

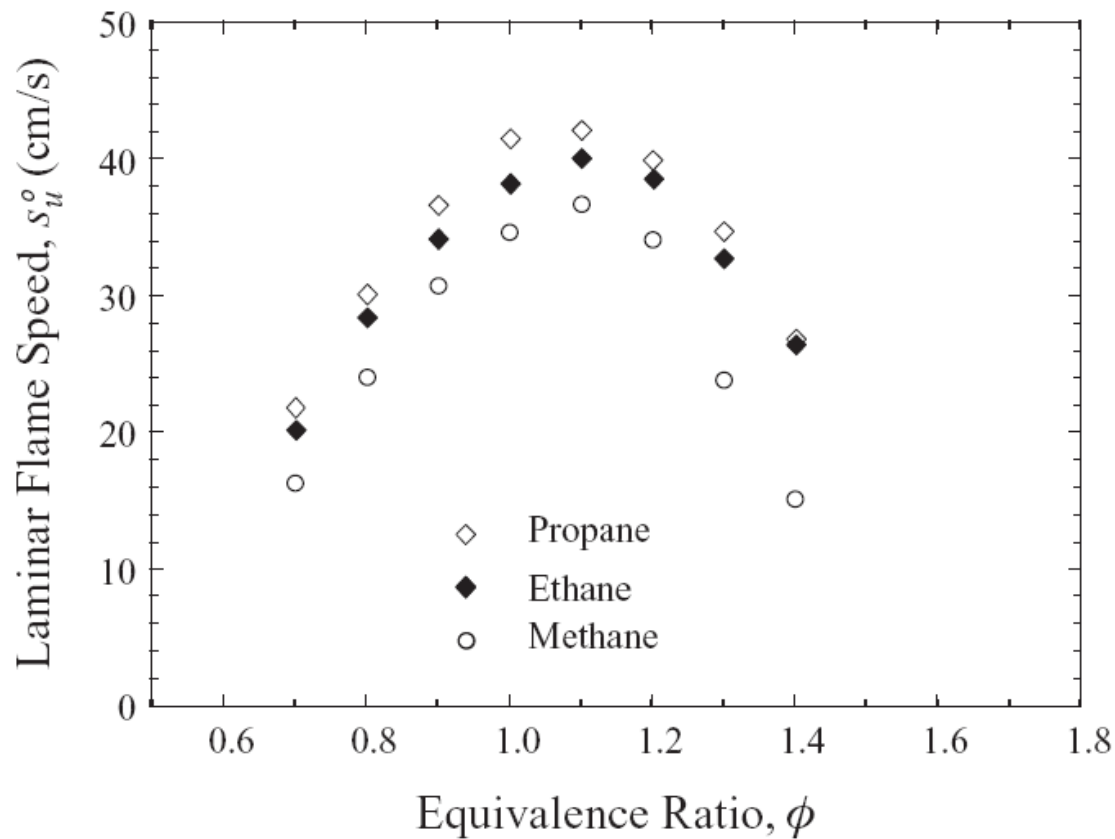
D : mass diffusion coefficient [m^2/s]

Ω : reaction rate [$1/\text{s}$]

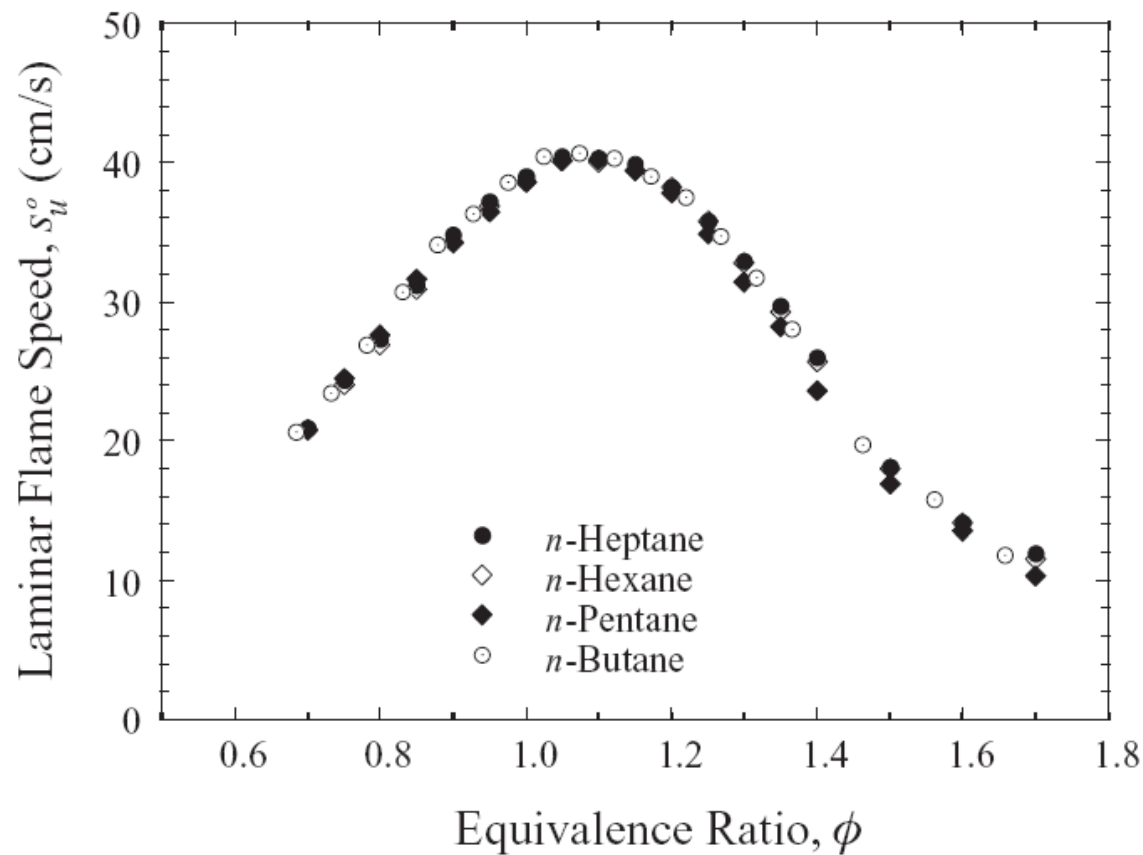
Dependence on fuel/air ratio



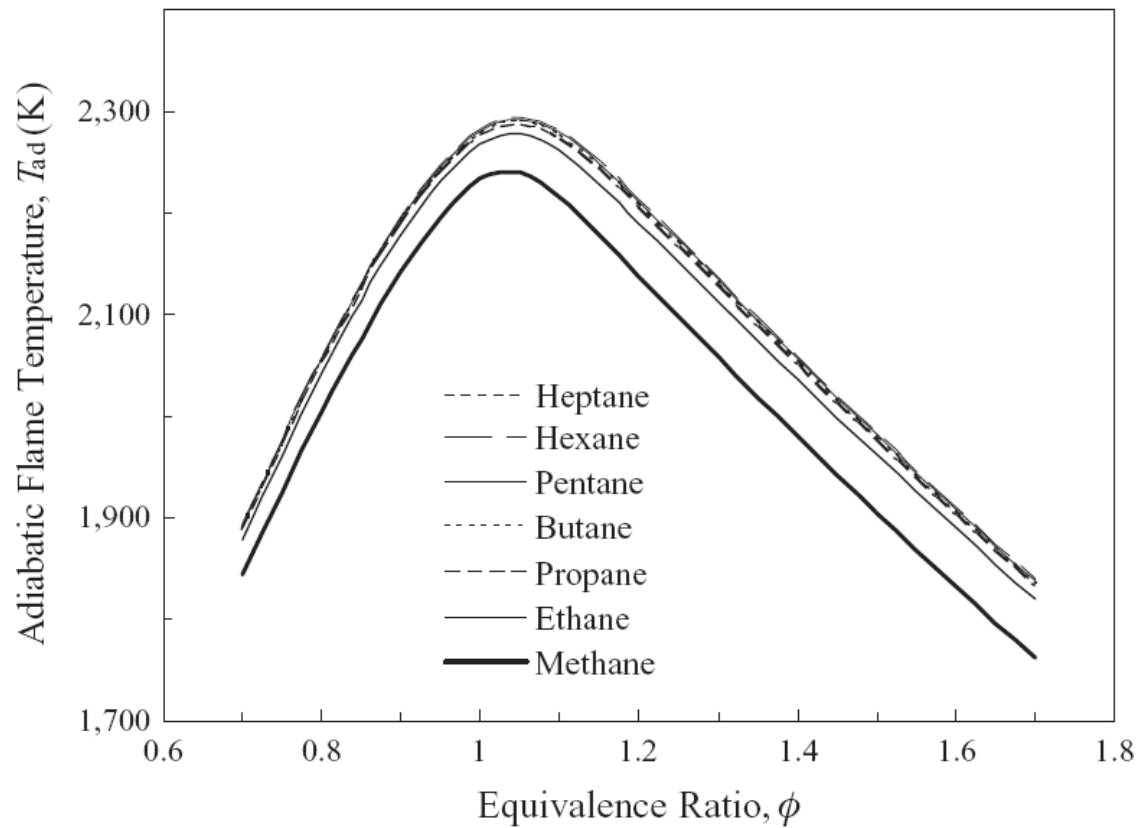
Dependence on flame temperature



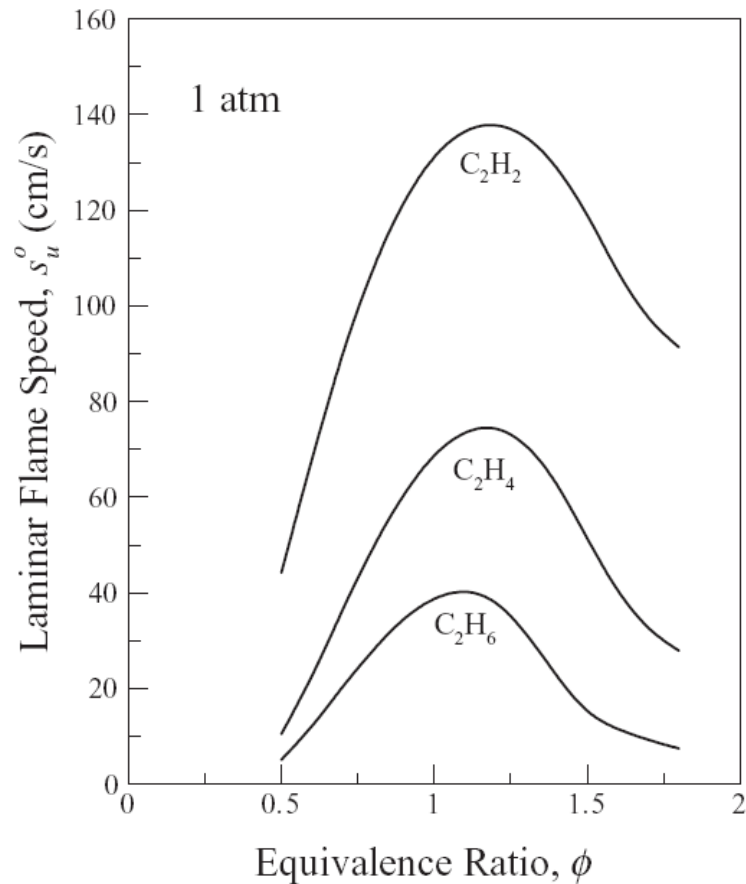
Dependence on flame temperature



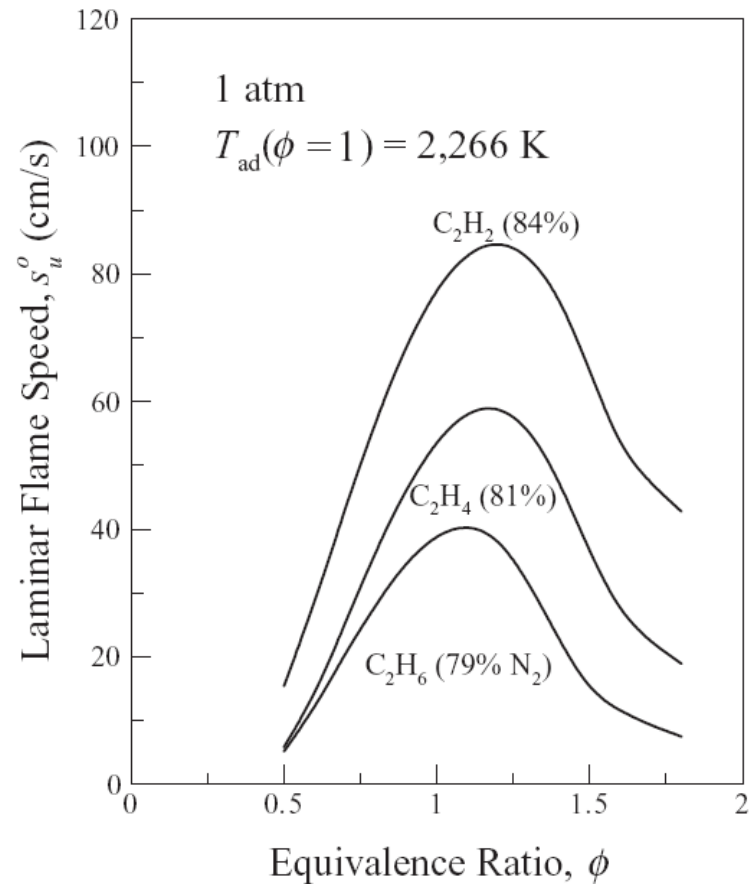
Dependence on flame temperature



Dependence on reactivity

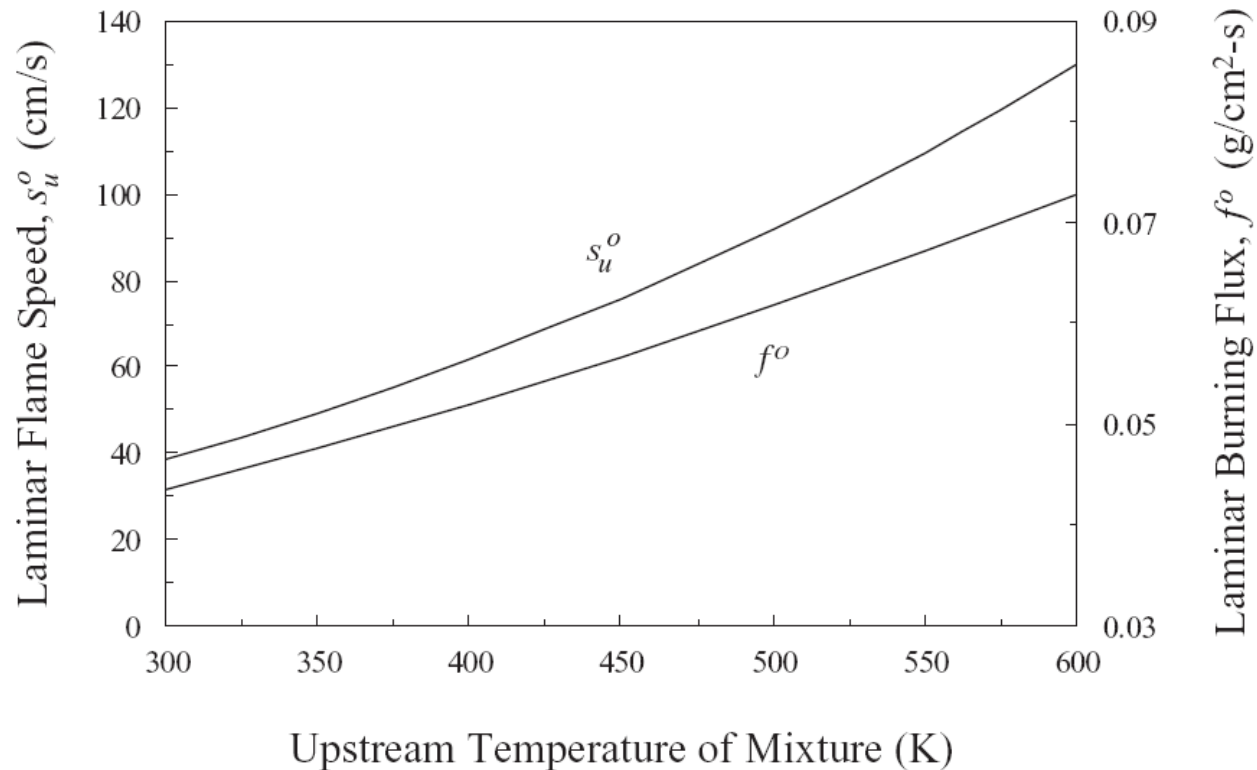


(a)

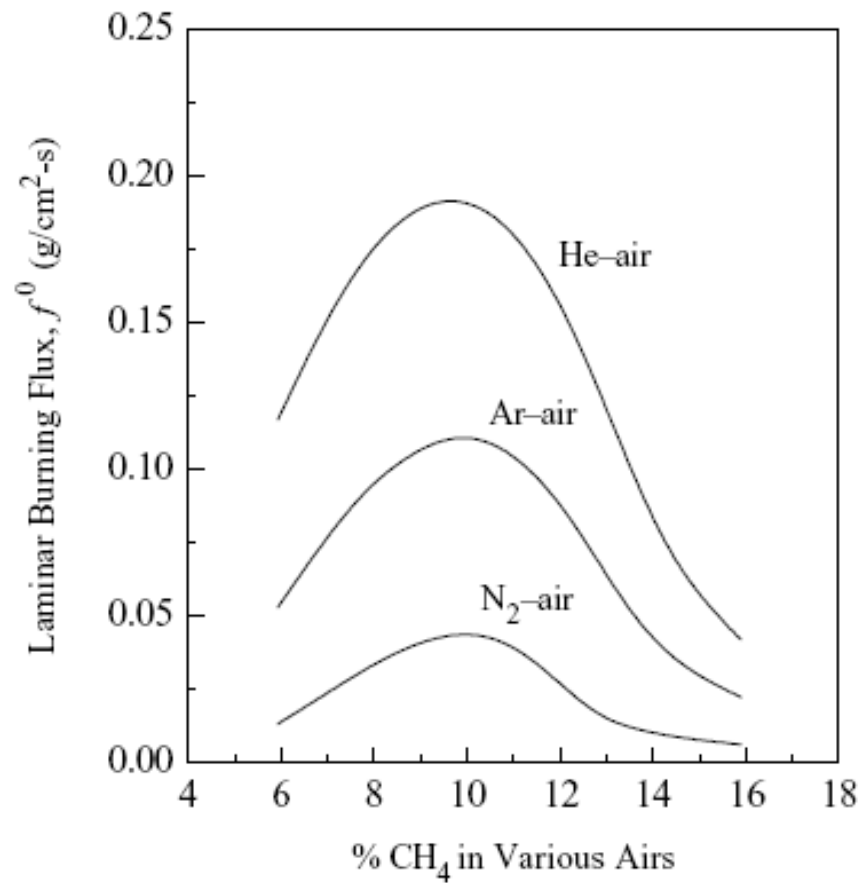


(b)

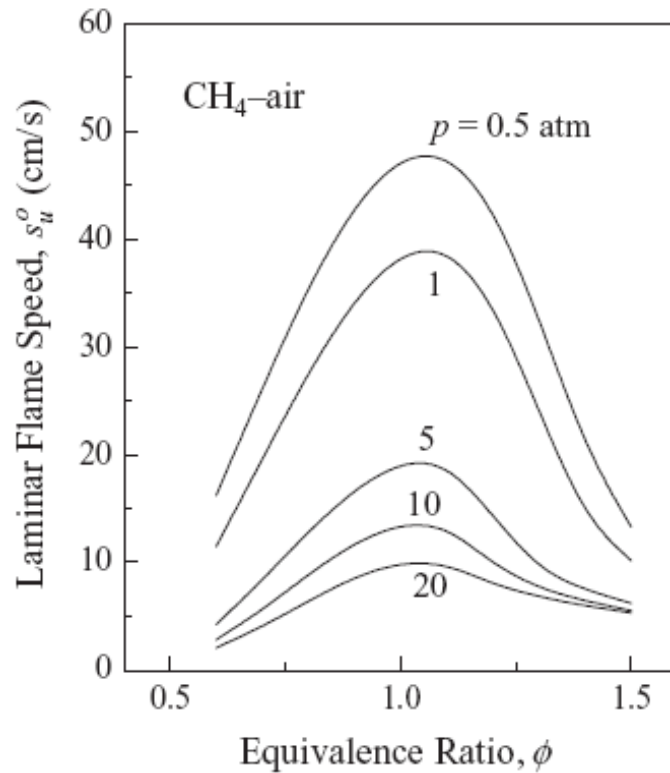
Dependence on preheat temperature



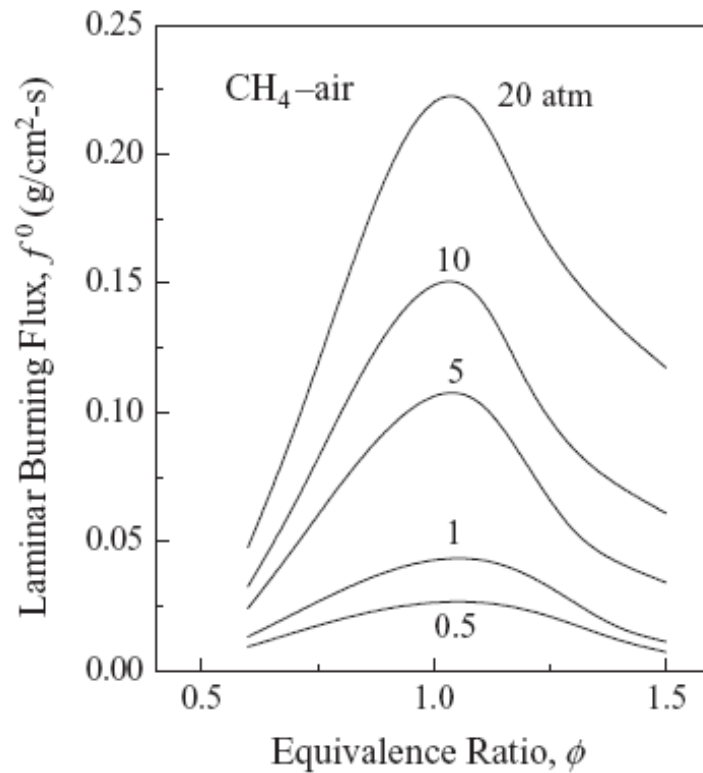
Dependent on transport properties



Dependence on pressure



(a)



(b)

Syngas/air (CO/H₂/air) flames

– effect of reactivity and diffusivity

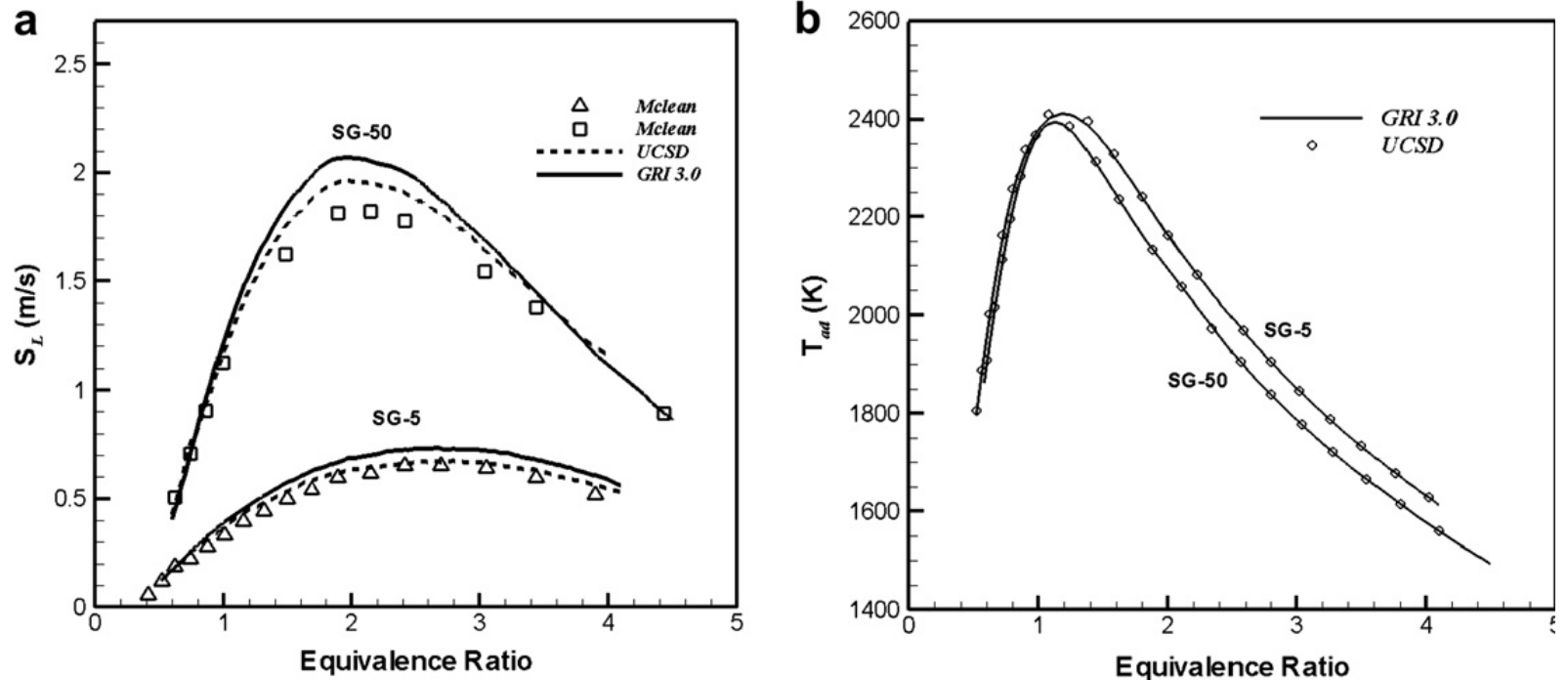
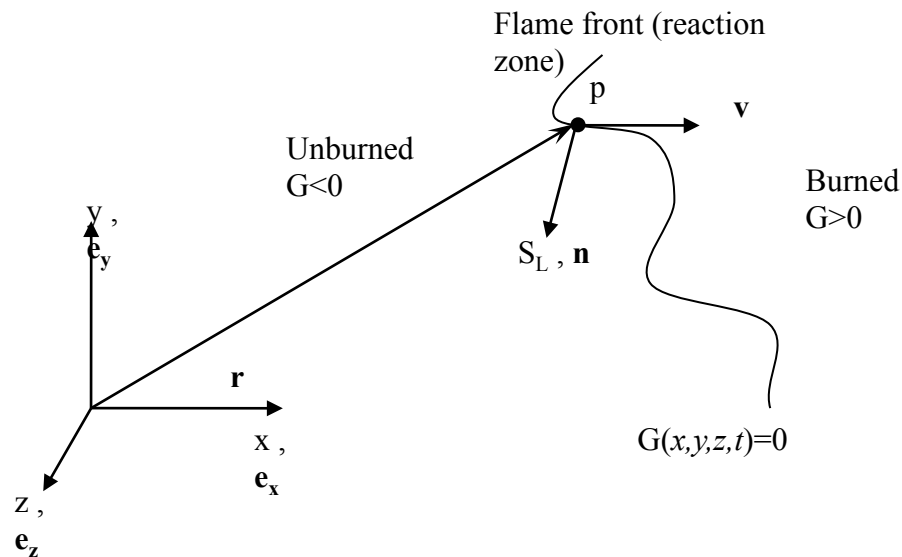


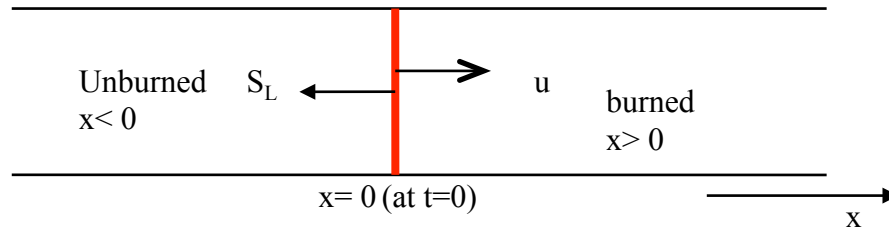
Fig. 10 – Laminar burning velocity and adiabatic flame temperature of syngas flames at atmospheric pressure and mixture temperature of 300 K.

Propagation of laminar premixed flame



$$\frac{\partial G}{\partial t} + \vec{v} \cdot \nabla G = S_L |\nabla G|$$

Planar flame in a pipe



- Stable flame
- Flash back
- Blow-off
- Wall effect

Bunsen flame

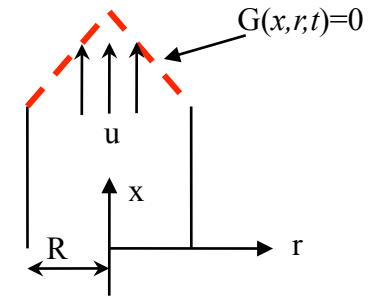
$$G(x, r, t) = x + f(r) = 0$$

$$u = S_L \sqrt{(f')^2 + 1}$$

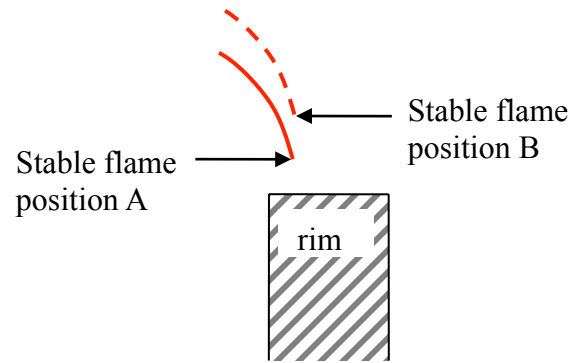
$$f(r) = \sqrt{\frac{u^2 - S_L^2}{S_L^2}} r + \text{constant}$$

$$x = (R - r) \sqrt{\frac{u^2 - S_L^2}{S_L^2}}$$

- Conical shape
- Flame length vs R , u , S_L



Bunsen flame stability



- Rim effect
- Lifted flame
- blowout

Stabilization of premixed flames

- Rim stabilization
- Pilot flame stabilization
- Bluff body stabilization